## COAL COMBUSTION RESIDUALS PRIMARY ASH POND PERIODIC HAZARD POTENTIAL CLASSIFICATION ASSESSMENT 5-Year Periodic Update

COLETO CREEK POWER PLANT FANNIN, TEXAS

October 11, 2021

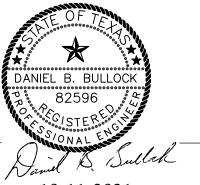


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# Certification Statement 40 C.F.R. § 257.73(a) and 30 T.A.C. § 352.731- Hazard Potential Classification Assessment

## CCR Unit: Coleto Creek Power, LLC; Coleto Creek Power Plant; Coleto Creek Primary Ash Pond

I, Daniel Bullock, being a Registered Professional Engineer in good standing in the State of Texas, do hereby certify, to the best of my knowledge, information, and belief that the information contained in this assessment report has been prepared in accordance with the accepted practice of engineering. I certify, for the above referenced CCR Unit, that the information contained in the Hazard Potential Classification Assessment, dated October 11, 2021, meets the requirements of 40 C.F.R. §257.73(a) and 30 T.A.C. § 352.731.



Daniel B. Bullock, P.E. (TX 82596)

10-11-2021

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#### **1.0 INTRODUCTION**

Coleto Creek Power Plant is located at 45 FM 2987 just outside the city of Fannin in Goliad County, Texas. The power plant consists of one coal-fired boiler. Bottom ash and fly ash, or coal combustion residuals (CCR), generated in the boiler are either shipped off-site for beneficial reuse or managed in an on-site CCR surface impoundment (Coleto Creek Primary Ash Pond). Figures 1 and 2 provide site location maps showing the Primary Ash Pond configuration.

In April 2015, the Environmental Protection Agency (EPA) promulgated rules (40 C.F.R. Part 257, Subpart D) to address potential risks associated with operating CCR surface impoundments at coal-fired power plants. The State of Texas subsequently codified 30 T.A.C. Chapter 352, which incorporated 40 C.F.R. §257 by reference, to address CCR management in surface impoundments and landfills. This report has been prepared to specifically address the requirements for periodic Hazard Potential Classification Assessments to be performed every 5 years as identified in 40 C.F.R. § 257.73(a)(2) and 30 T.A.C. § 352.731.

#### 2.0 PERIODIC HAZARD POTENTIAL CLASSIFICATION ASSESSMENT

According to 30 T.A.C. § 352.731 and 40 C.F.R. § 257.73(a)(2) by reference, the owner and operator of a CCR surface impoundment must assign a hazard potential classification to each operating unit. For the purposes of the CCR rule, hazard potential classification means "the possible adverse incremental consequences that result from the release of water or stored contents due to failure of the diked CCR surface impoundment or mis-operation of the diked CCR surface impoundment or its appurtenances." The impoundment must be classified as high hazard, significant hazard, or low hazard. Each hazard potential classification is defined as follows under § 257.53:

- 1) *High hazard potential CCR surface impoundment* means a diked surface impoundment where failure or mis-operation will probably cause loss of human life.
- Low hazard potential CCR surface impoundment means a diked surface impoundment where failure or mis-operation results in no probable loss of human life and low economic and/or environmental losses. Losses are principally limited to the surface impoundment owner's property.
- 3) *Significant hazard potential CCR surface impoundment* means a diked surface impoundment where failure or mis-operation results in no probable loss of human life, but can cause economic loss, environmental damage, disruption of lifeline facilities, or impact other concerns.

In 2010 the United States Environmental Protection Agency (USEPA) contracted CDM to perform a site assessment of the Primary Ash Pond at the Coleto Creek Power Plant. As part of the assessment, CDM assigned the pond with a Low Hazard classification (CDM, 2011).

Subsequent to the CDM report findings, AECOM was contracted by the plant to perform geotechnical studies to further evaluate the structural stability of the CCR surface impoundments. AECOM implemented a subsurface investigation and performed a geotechnical stability evaluation, a liquefaction assessment, and hydraulic analysis. AECOM also performed an independent hazard assessment of the Primary Ash Pond and Secondary Pond. The results of that assessment supported the initial CDM classification of Low Hazard. The initial Potential Hazard Class assessment performed in 2016 in accordance with the federal CCR rules also concluded that the Primary Ash Pond is a Low Hazard surface impoundment (BBA, 2018).

#### 2.1 Dam Breach Analysis

The Coleto Creek Primary Ash Pond is the only CCR-regulated surface impoundment at the Coleto Creek Power Plant and is therefore subject to the Hazard Potential Classification Assessment under the CCR rules. Because the Primary Ash Pond is hydraulically connected to, and is separated by a dike system from, the Secondary Pond, it is necessary to include the Secondary Pond when evaluating potential failure scenarios as noted below. Although the Secondary Pond is not a CCR-regulated unit, it is subject to operational and safety standards established by the Texas Commission on Environmental Quality (TCEQ) in its Dam Safety rules (30 T.A.C. Part 1 Chapter 299).

Bullock, Bennett & Associates (BBA) performed a dam breach analysis of the Primary Ash Pond and Secondary Pond to support the loss of life, and environmental and economic impact analyses. The Primary Ash Pond and Secondary Pond combined have a maximum storage capacity of approximately 4,000 acre-ft and a maximum dike height for the Secondary Pond of approximately 39 feet above adjacent lake level of 101 feet MSL. Construction was completed in 1978 and the effective water storage capacity in the Primary Ash Pond has diminished with the placement of CCR over time. According to topography and bathymetric survey data collected in August 2021, the water storage capacity in the Primary Ash Pond has been reduced to approximately 1,390 acre-ft at the maximum dike crest height while the water capacity of the Secondary Pond is estimated at 200 acre-ft.

The Primary Ash Pond and Secondary Pond are located next to the Coleto Creek Reservoir which was constructed to serve as a cooling pond for the Power Plant. The reservoir is divided into a "hot" side and a "cool" side. The ponds are located immediately adjacent to the hot side of the lake. The hot side of the lake is created from Sulphur Creek behind Dike No. 1 (Dike No. 1 Lake) which is connected to Turkey Creek behind Dike No. 2 (Dike No. 2 Lake) by a secondary flume. Water from these lakes then flows into Main Lake which is the cool side. Decant water from the Secondary Pond can be combined with other plant water then routed through TCEQ-approved Outfall 003 to the hot side of the lake. Cool water is pumped into the Power Plant from the Main Lake.

GBRA provided area-capacity tables for the Coleto Creek Reservoir and Dike Lake Nos. 1 and 2. These tables are presented as attachments in Appendix A. Dike No. 1 Lake consists of approximately 164 acres at the normal operating elevation of 101 feet MSL. Dike No. 2 Lake is approximately 429 acres at the normal operating elevation of 101 feet MSL. The two Dike Lakes are separated from Coleto Creek Reservoir by splitter dikes with an approximate elevation of 102 feet MSL (GBRA, 2016). Coleto Creek Reservoir covers an area of approximately 2,652 acres at a normal operating elevation of 98 feet MSL (GBRA, 2016). Coleto Creek Power, LLC reportedly controls the lake up to an elevation of 104 feet MSL. An area map showing the relative locations of the Primary Ash Pond, Secondary Pond, Dike Lakes, and Coleto Creek Reservoir is presented as Figure 1.

For the purposes of this evaluation, a conservatively worst-case dam breach scenario was developed assuming that the breach was due to overtopping of the surface impoundment dikes and that the breach occurs in the shared Primary Ash Pond and Secondary Pond dike and subsequently in the Secondary Pond dike adjacent to Coleto Creek Reservoir, releasing the entire water contents of both ponds. This scenario allows for the greatest quantity of pond decant water to be released.

An evaluation of potential water and residual solids flow paths was performed to support the loss of life, environmental, and economic evaluations. Surface elevation cross-sections assembled from Google Earth<sup>TM</sup> profiles of the areas adjacent to the pond dikes were reviewed to estimate the potential flow path of the released water and solids. As shown in Figure 1, the wet side of the ponds are bound by the Evaporation Pond followed by Dike No. 1 Lake on the northnorthwest, Dike No. 1 Lake on the northeast corner, and the primary plant discharge flume on the east. The surface elevation of the terrain that bounds the east side of the discharge flume appears to extend to approximately elevation 132 feet. The flume channel, therefore, appears to be located within a larger basin bounded to the west by the Primary Ash Pond and Secondary Pond dikes (approximate elevation 140 feet) and to the east by land mass (approximate elevation 132 feet). The distance between the dike on the west side of the basin and land mass high points on the east side appears to be approximately 300 feet. The flume channel and basin would route flow from an east-side breach of the dike to the hot side of the lake. Released water and solids, therefore, would initially flow to the hot side of the lake regardless of the location of the breach. From there, water levels would increase one foot (the amount of available freeboard behind Dike No. 1 and Dike No. 2 lakes) then flow into the Main Lake. Eventually all water would be released into the Main Lake.

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Using the tables provided by GBRA, a one-foot increase in the Main Lake elevation requires an additional approximately 2,720 acre-feet of water. The estimated maximum volume of discharge from the Primary Ash Pond and Secondary Pond is approximately 1,590 acre-feet of water, resulting in a water surface elevation change on the reservoir of approximately seven inches. A seven-inch change in water surface elevation is considered to be nominal and would not result in the loss of major infrastructure elements or disrupt lifeline facilities.

#### 2.2 Loss of Life Evaluation

The Primary Ash Pond and Secondary Pond are located apart from the active industrial areas of the Power Plant. Two fly-ash silos are located adjacent to the southwest border of the Primary Ash Pond and loading of trucks for off-site transport and beneficial reuse of the fly ash regularly occurs at this location. These silos and truck loading operations are adjacent to the southwest limits of the Primary Ash Pond, which is filled with dry and compact CCRs, and any catastrophic failure of the impoundment in this area is unlikely. If a failure were to occur, it would probably be located on the "wet" side of the pond, including the northern or eastern dikes for both the Primary Ash Pond and Secondary Pond (see Figure 1). There are no regular or active plant operations that occur downstream of those areas where personnel would be expected to be present in the event of a catastrophic failure of the dike. There are no residences or other off-site manned operations immediately downstream of the ponds. As noted in Section 2.1 the Dike 1, Dike 2, and Main Lakes would absorb the released water and raise reservoir levels a nominal amount (less than a foot). Loss of life in the event of a catastrophic failure and raise reservoir levels a nominal amount (less than a foot). Loss of life in the event of a catastrophic failure of the surface impoundment dike system, therefore, is considered to be improbable.

#### 2.3 Economic and/or Environmental Loss Evaluation

Additional consideration was given to the impacts of the water quality from a large volume discharge from Primary Ash Pond and Secondary Pond into the Coleto Creek Reservoir. Using the volume ratio of pond water (approximately 1,590 acre-feet) that could potentially be discharged into the Coleto Creek Reservoir to the existing volume of water in the reservoir (approx. 31,280 acre-feet at elevation 98 feet msl), the impacts to the water quality are minimal (31,280 acre-feet/1,590 acre-feet =  $\sim$ 20 dilution factor of analytes in the Primary Ash Pond water). Discharge of Secondary Pond water is currently allowed to the Coleto Creek Reservoir under Permit No. WQ002159000 (TCEQ, 2010).

Currently, the coal combustion by-products are sluiced into the Primary Ash Pond. The assumed ratio of solids-to-water is approximated at 20%-to-80%. The solids settle out of solution and the water decants to the surface. As the solids settle out of solution, they consolidate. Additionally, based on field observations the ash "sets up" similar to cement, becoming very hard and massive. The expected flow of any unconsolidated solids from the Primary Ash Pond is believed to be minimal.

For the sake of conservatism, it is assumed that a volume of ash equivalent to six months of production (assuming no recycling) is disposed in the Primary Ash Pond that may not be consolidated and may flow should a breach occur. Under these assumptions, there is potential for approximately 45,000 cubic yards (approximately 28 acre-feet) of ash flow. The ash volume would be in solution with the decant water, displacing an equal volume of the decant water. This ash would be expected to be contained within the hot side of the lake. Impacts would therefore be primarily limited to the owner's property.

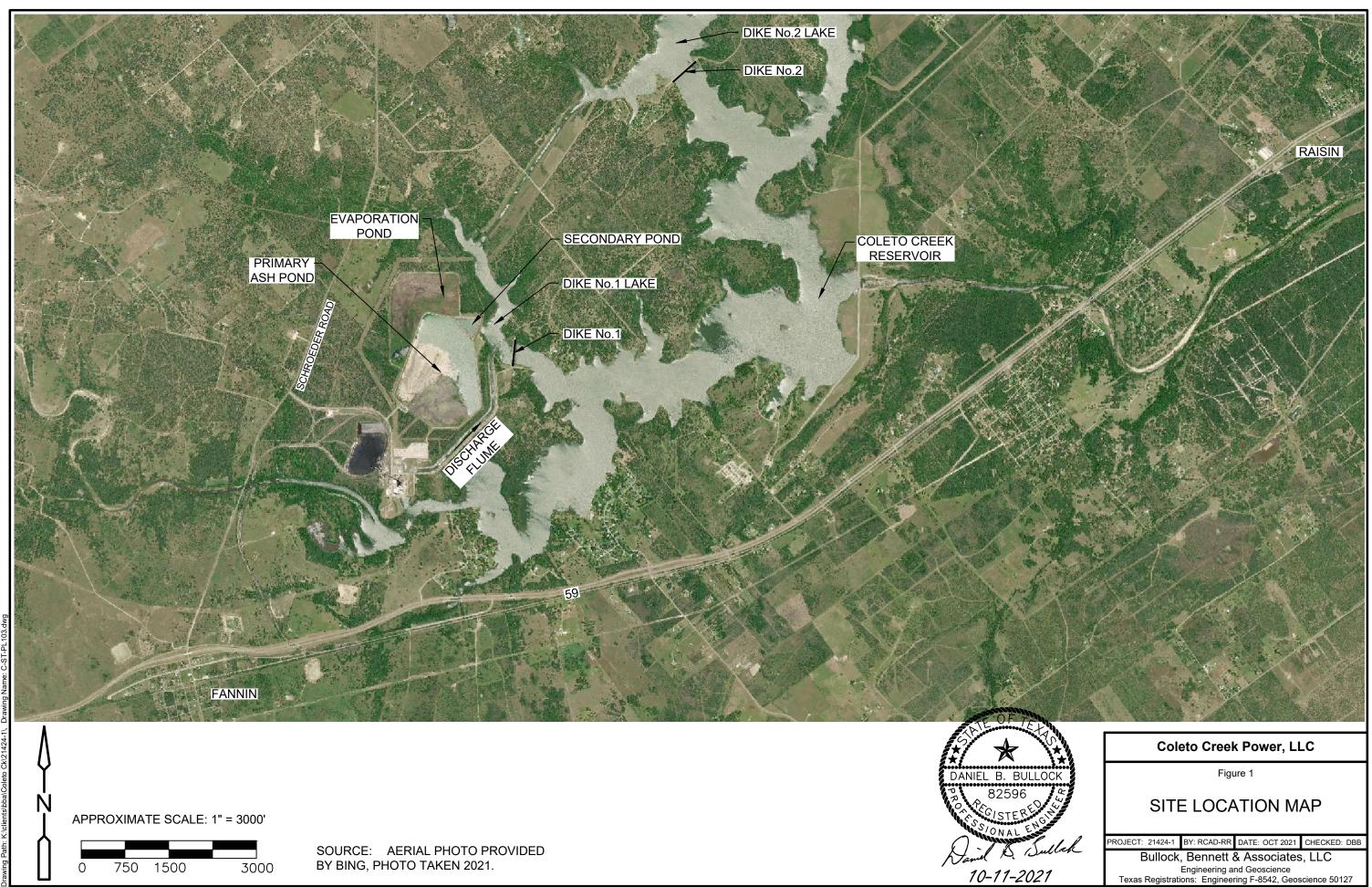
#### 2.4 Hazard Potential Classification

Based on a review of previous studies, analytical data, ash production/recycling volumes, available impoundment capacities, available lake capacities, observed current conditions at the site, assumptions, and other factors, the Coleto Creek Primary Ash Pond is classified as a Low Hazard Potential impoundment.

#### **3.0 REFERENCES**

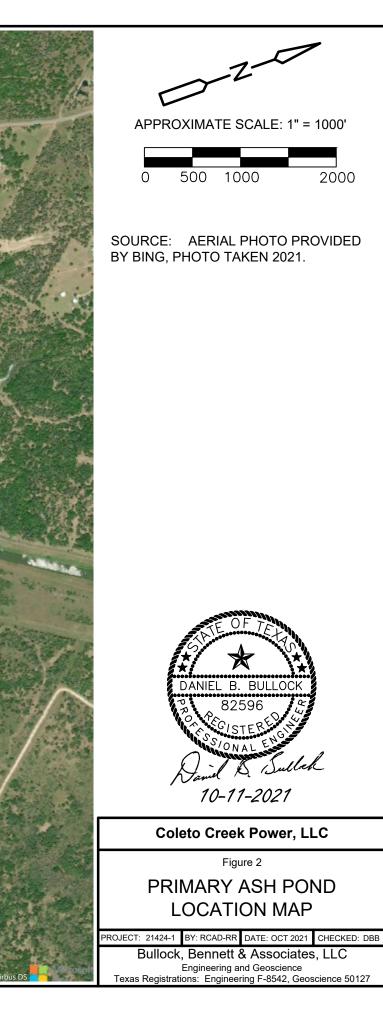
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## FIGURES



Plot Date: 10/11/21 - 1:23pm, Plotted by: Admin Drawing Path: K:\clients\bba\Coleto Ck\21424-1\. Drawing Name: C-





## **APPENDIX A**

Guadalupe-Blanco River Authority Lake Area-Capacity Summaries

TAB	LE	1

COLETO CREEK RESERVOIR AREAS AND CAPACITIES INITIAL CONDITIONS\*

Elev	. 0	1	2	3	4	5	6	7	8	9	
	AREA IN ACRES										
50									0	9	
60	18	26	34	42	50	60	80	100	120	145	
70	170	200	239	277	314	351	397	442	495	547	
80	599	679	758	835	910	984	1087	1189	1299	1408	
90	1504	1650	1796	1940	2084	2230	2369	2514	2652	2787	
100	2918	3077	3255	3461	3698	3954	4207	4458	4706	4949	
110	5190	5531	5910	6324	6763	7234	7734	8229	8725	9223	
120	9723										
	CAPACITY IN ACRE-FEET										
										•	
50									0	. 4	
60	18	40	70	108	154	209	279	369	479	611	
70	769	954	1174	1432	1727	2060	2434	2853	3322	3843	
80	4416	5055	5774	6570	7442	8389	9425	10,563	11,807	13,160	
90	14,617	16,194	17,917 43,012	19,786	21,798 49,949	23,955 53,744	26,254	28,695 62,187	31,277 66,769	33,996 71,597	
$\begin{array}{c} 100 \\ 110 \end{array}$	36,849 76,667	39,846 82,027	43,012	46,370 93,863	100,406	107,409	114,807	122,878	131,354	140,328	
120	149,800	02,027	07,747	55,005	100,400	107,405	117,007	122,070	101,004	140,020	
100	1,0,000										

\*Areas and capacities of impoundments behind Dike Nos. 1 and 2 are not included in this tabulation.

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### TABLE 2

### COLETO CREEK PROJECT AREAS AND CAPACITIES SULPHUR CREEK BEHIND DIKE NO. 1 INCLUDING FLUME NO. 1

Elev.	0	1	. 2	3	4	5	6	7	8	9	
AREA IN ACRES											
70 80 90 100 110 120	3 49 151 329 770	56 164 358	7 64 178 388	10 73 193 419	14 82 207 455	18 90 223 499	22 101 240 540	0 26 113 259 590	1 31 126 279 641	2 36 138 303 699	
CAPACITY IN ACRE-FEET											
70 80 90 100 110 120	4 199 1141 3429 8570	8 251 1299 3773	14 311 1470 4146	23 379 1656 4550	35 456 1856 4987	51 542 2071 5464	71 638 2303 5984	95 745 2553 6549	0 123 865 2822 7165	2 157 997 3113 7835	

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### TABLE 3

### COLETO CREEK PROJECT AREAS AND CAPACITIES TURKEY CREEK BEHIND DIKE NO. 2 INCLUDING FLUME NO. 2

Elev	. 0	1	2	3	4	5	6	7	8	9	
14 1	an an Arian An Ariana an Arian		· · · · · · · · · · · · · · · · · · ·	· · · ·	AREA II	N ACRES					
70 80 90 100 110 120	38 167 391 791 1537	0 46 184 429 - 831	1 55 200 467 882	3 65 217 506 947	6 76 234 545 1032		623	293 663	24 130 322 705 1374	31 146 355 748 1458	
				CAP	ACITY II	ACRE-1	FEET			- -	
70 80 90 100 110 120	124 1048 3654 9513 20,819	4064	1416 4512	2 276 1624 4998 12,096	5524	14 429 2092 6089 14,161	523 2352 6691	41 631 2634 7334 16,572	62 754 2942 8018 17,905	892 3281 8744	

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